

The CoMP-S@LSO: polarimetric calibration

Jan Rybak, Steve Tomczyk, the LSO group



AISAS colloquium, TL, 2024/03/20

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- CoMP-S polarimetric calibration procedure
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- A proposal for a new CoMP-S polarimetric package

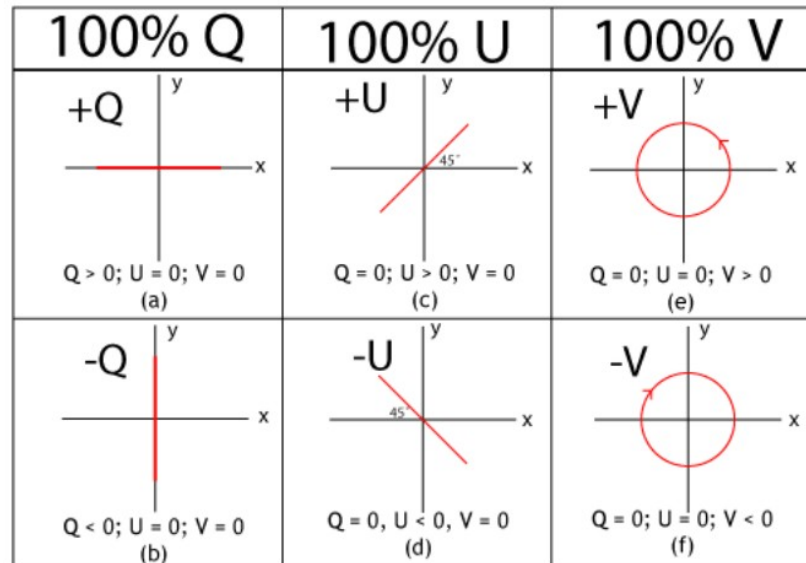
Polarimetry as a tool

- Polarimetry - measurements of the polarization properties of the light
- Polarization of the measured light – result of the magnetic field surrounding the atoms emitting the observed light:
 - Only some atom transitions
 - The Zeeman and Hanle effects
 - (other physical effects)
- We can not measure polarization, we can measure only intensity...
- Approaches for measurements:
 - Sequential measuring of different individual pol. states
 - Sequential measuring of different combinations of the individual pol. states

Polarimetry as a tool

- The polarized light descriptions:
 - The Poincare sphere, the Jones vector
 - **The Stokes vector [I,Q,U,V]:** the standard Cartesian basis (x, y), the Cartesian basis rotated by 45° (a,b), and a circular basis (l, r), E – the el. field amplitude

$$\begin{aligned}
 I &\equiv \langle E_x^2 \rangle + \langle E_y^2 \rangle \\
 &= \langle E_a^2 \rangle + \langle E_b^2 \rangle \\
 &= \langle E_r^2 \rangle + \langle E_l^2 \rangle, \\
 Q &\equiv \langle E_x^2 \rangle - \langle E_y^2 \rangle, \\
 U &\equiv \langle E_a^2 \rangle - \langle E_b^2 \rangle, \\
 V &\equiv \langle E_r^2 \rangle - \langle E_l^2 \rangle.
 \end{aligned}$$



Wikipedia: https://en.wikipedia.org/wiki/Stokes_parameters

Instrumental polarization

- All optical parts of your instrument might alter (modulate) the polarimetric status of the light to be measured
- Your instrument as a whole: **O - modulation matrix** ($n_{\text{meas}} \times 4$)

$$\mathbf{I}_{\text{meas}} = \mathbf{O} \mathbf{I}_{\text{in}} \quad \mathbf{I} \equiv (I, Q, U, V)^T$$

$$\mathbf{O} = \begin{pmatrix} I_{\text{in}} \rightarrow I_{\text{meas}} & Q_{\text{in}} \rightarrow I_{\text{meas}} & U_{\text{in}} \rightarrow I_{\text{meas}} & V_{\text{in}} \rightarrow I_{\text{meas}} \\ I_{\text{in}} \rightarrow Q_{\text{meas}} & Q_{\text{in}} \rightarrow Q_{\text{meas}} & U_{\text{in}} \rightarrow Q_{\text{meas}} & V_{\text{in}} \rightarrow Q_{\text{meas}} \\ I_{\text{in}} \rightarrow U_{\text{meas}} & Q_{\text{in}} \rightarrow U_{\text{meas}} & U_{\text{in}} \rightarrow U_{\text{meas}} & V_{\text{in}} \rightarrow U_{\text{meas}} \\ I_{\text{in}} \rightarrow V_{\text{meas}} & Q_{\text{in}} \rightarrow V_{\text{meas}} & U_{\text{in}} \rightarrow V_{\text{meas}} & V_{\text{in}} \rightarrow V_{\text{meas}} \end{pmatrix}$$

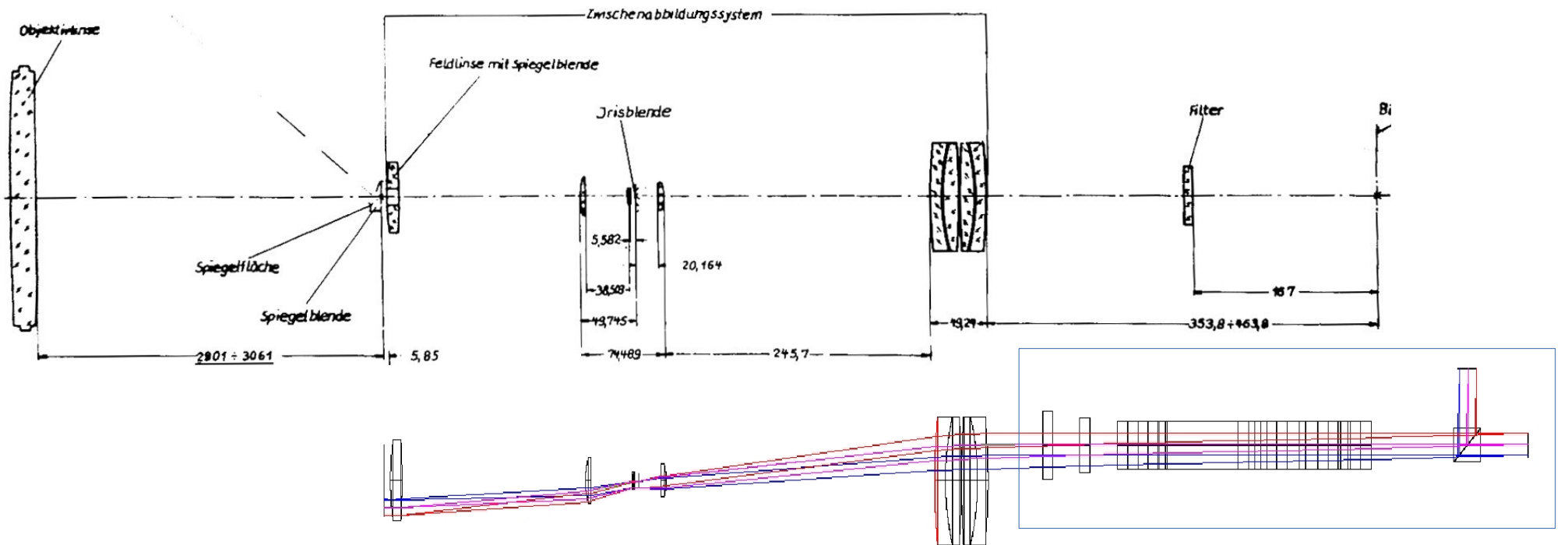
- This modulation of the light polarimetric status has to be determined in form of the **O** modulation matrix = the polarimetric calibration

Polarimetric calibration

- Method:
 - IN - known polarimetric status
 - OUT – measured polarimetric response to IN
 - O_{ij} – determination from IN and OUT using an instrument description
- Approaches for measurements:
 - Sequential measuring of individual pol. states (+Q,-Q,+U,...)
 - **Sequential measuring of different combinations of the individual pol. states**

CoMP-S as polarimeter

- The CoMP-S instrument and the ZEISS 200/3000/4000 coronagraph



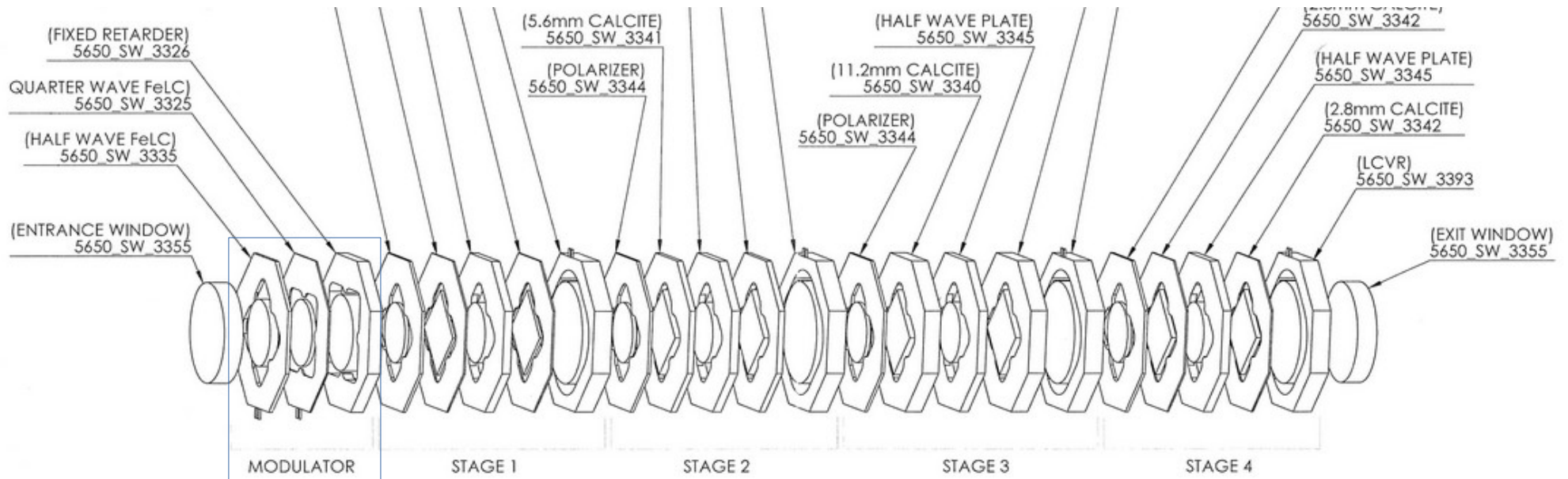
Coronagraph & primary optics

Coronagraph secondary optics

& CoMP-S instrument + tertiary optics

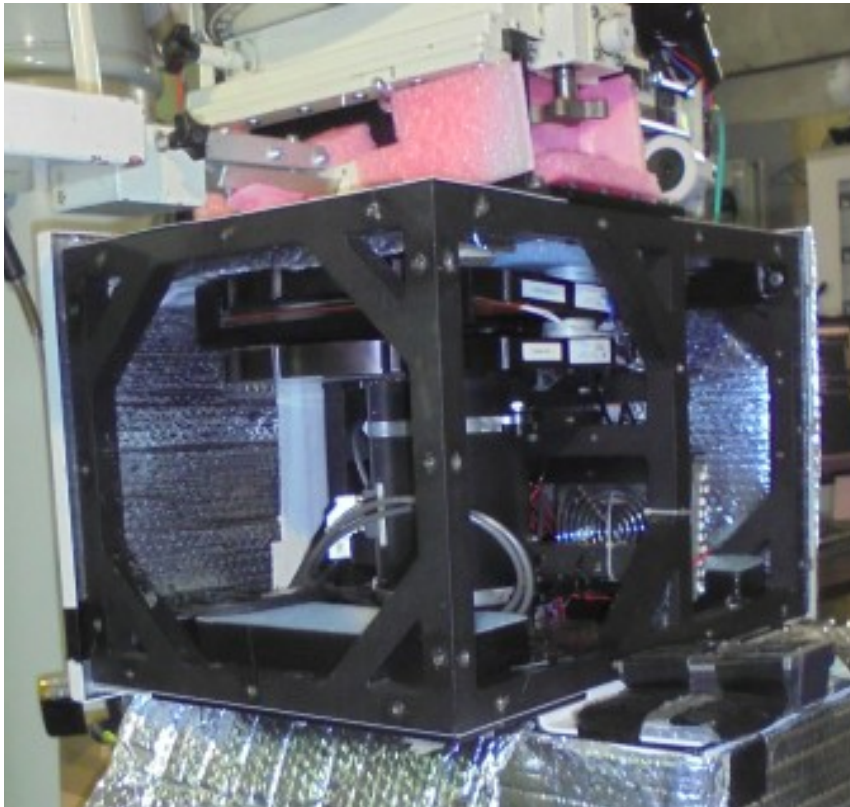
CoMP-S as polarimeter

- The CoMP-S instrument: 4-stage tunable Lyot filter + polarimeter
- Polarimeter: a half-wave plate + a quarter-wave plate + a fixed retarder
- Wave plates: Ferroelectric liquid crystals (DISPLAYTECH, # LV2500), external el. field ± 5 VDC \rightarrow 4 alternations of the passing light polarization state change (retardation) is wavelength dependent



CoMP-S pol. calibration

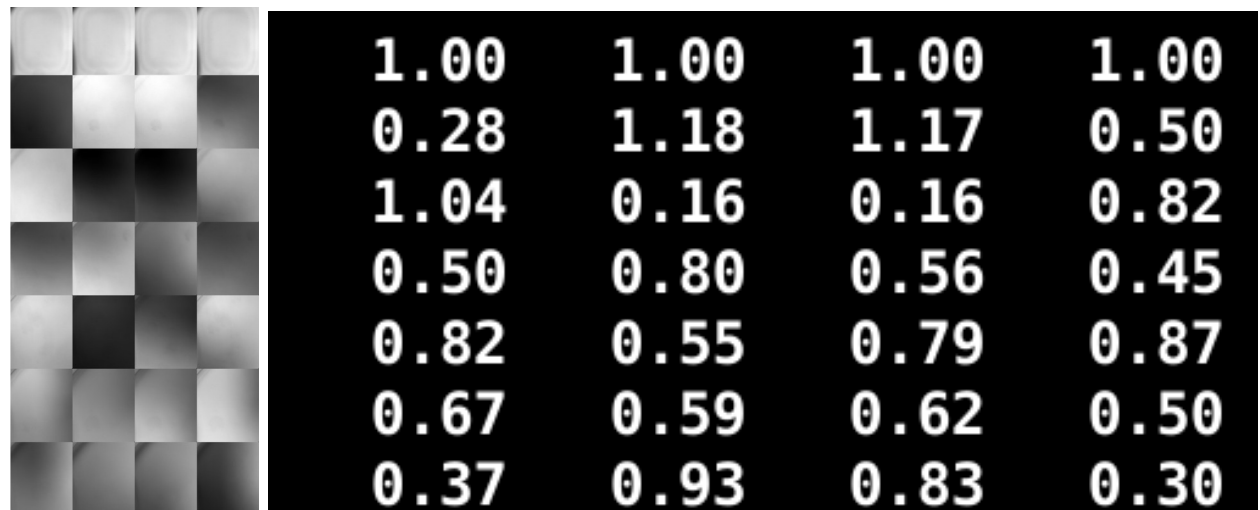
- Polarimetric calibration: IN – light of known polarimetric status:
 - polarimetric optics in the calibration wheel: CLEAR, lin. polarizer @ 0° , 90° , 45° , -45° ; lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder @ $+45^\circ$; lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder @ -45°



CoMP-S pol. calibration

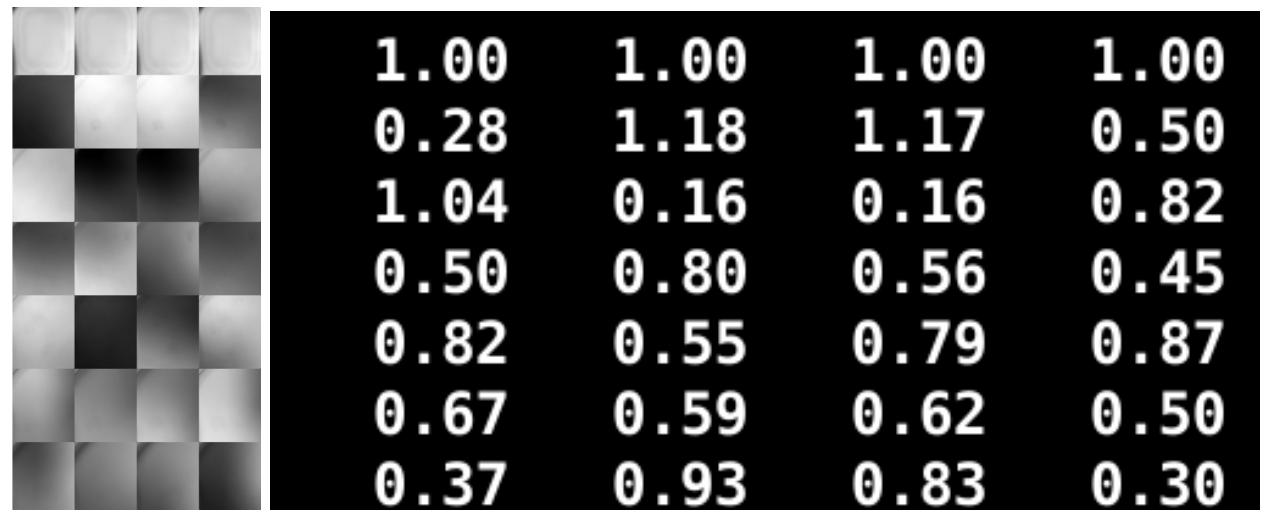
- Polarimetric calibration: OUT – response to the light of known polarimetric status passing the instrument:
 - Horizontal: polarimeter - 4 FLC combinations in the CoMP-S
 - Vertical: calibration optics - CLEAR, lin. polarizer @ 0° , 90° , 45° , -45° ; lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder @ $+45^\circ$; lin. polarizer 0° + $\frac{1}{4}$ wave retarder @ -45°
 - Example for 656.16 nm (FWHM ~ 0.05 nm): 2D images & 1 point

I_{meas} matrix:



CoMP-S pol. calibration

- Procedure for the determination of the \mathbf{O} matrix from the measured response of the instrument \mathbf{I}_{meas} to the input light of the known pol. states is inevitable
- A more sophisticated approach: a polarimetric model of the instrument with some free parameters to be adjustable in order to describe the instrument as good as possible. Reasons for this approach: optical properties of the pol. parts (transmission & retardation \sim wavelength, FoV spatial variations)



CoMP-S pol. calibration

- The polarimetric model of the CoMP-S instrument:
 - Parameters (initial guess):
 - Input light Stokes vector $[I, Q, U, V]$ ($I_{\text{mean}}, 0, 0, 0$)
 - linear polarizers (free: transmission (0.5), fixed: pol. ratio, orientation)
 - $\frac{1}{4}$ wave retarder (free: transmission (1.0), retardation ($90. * \text{wave}_{\text{norm}}$), fixed: orientation)
 - O matrix:

$$\begin{bmatrix} I_{\text{meas}}(0,1)-I_{\text{meas}}(0,2))/2., (I_{\text{meas}}(0,3)-I_{\text{meas}}(0,4))/2., (I_{\text{meas}}(0,5)-I_{\text{meas}}(0,6))/2. \\ I_{\text{meas}}(1,1)-I_{\text{meas}}(1,2))/2., (I_{\text{meas}}(1,3)-I_{\text{meas}}(1,4))/2., (I_{\text{meas}}(1,5)-I_{\text{meas}}(1,6))/2. \\ I_{\text{meas}}(2,1)-I_{\text{meas}}(2,2))/2., (I_{\text{meas}}(2,3)-I_{\text{meas}}(2,4))/2., (I_{\text{meas}}(2,5)-I_{\text{meas}}(2,6))/2. \\ I_{\text{meas}}(3,1)-I_{\text{meas}}(3,2))/2., (I_{\text{meas}}(3,3)-I_{\text{meas}}(3,4))/2., (I_{\text{meas}}(3,5)-I_{\text{meas}}(3,6))/2. \end{bmatrix} / I_{\text{mean}}$$
 - Definitions of the polarimetric calibration optics (type, orientation)
 - Calculation of the calibration optics impact on the passing light (in form of the Mueller matrices)

CoMP-S pol. calibration

- The polarimetric model of the CoMP-S instrument:
 - Fitting the model parameters to reach the minimum of the user-written function = sum of intensity differences $(I_{\text{meas}} - I_{\text{model}})^2$
 - The IDL procedure **POWELL**: based on powell code for minimization in N-dimensions (*section 10.5 of Numerical Recipes in C: The Art of Scientific Computing (Second Edition), Cambridge University Press, 1992*)
 - Typical IDL performance for our data: 19 parameters, 28 measurements, 15-50 iterations to reach the 10^{-6} limit, normalized $\chi^2 < 0.01$, runtime $\sim 10^{-1}$ s
 - The parameters used to clarify appropriateness of the model:
 - normalized $(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$ intensity differences
 - reliability of the obtained values of the physical parameters: linear polarizer transmission, circular retarder transmission & retardation Stokes_input vector, efficiencies (and other additional parameters)

CoMP-S pol. calibration

- The polarimetric model of the CoMP-S instrument:
 - normalized $(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$ intensity differences measure

Horizontal: polarimeter - 4 FLC combinations in the CoMP-S

Vertical: calibration optics - CLEAR, lin. polarizer @ 0° , 90° , 45° , -45° ; lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder @ $+45^\circ$; lin. polarizer 0° + $\frac{1}{4}$ wave retarder @ -45°

I_{meas}

$(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$

1.00	1.00	1.00	1.00
0.28	1.18	1.17	0.50
1.04	0.16	0.16	0.82
0.50	0.80	0.56	0.45
0.82	0.55	0.79	0.87
0.67	0.59	0.62	0.50
0.37	0.93	0.83	0.30

0.001	0.001	0.004	-0.007
-0.014	-0.145	-0.023	0.104
0.036	0.065	-0.009	-0.110
-0.008	0.010	0.025	0.002
-0.013	0.034	0.011	0.002
0.044	0.187	0.002	-0.543
0.040	0.342	0.002	-0.561

CoMP-S pol. calibration

- The polarimetric model of the CoMP-S instrument:
 - Resulting O matrix:

1.00	-0.58	-0.07	0.28
1.00	0.72	0.73	-0.01
1.00	0.73	0.50	0.07
1.00	-0.29	-0.05	0.38

$$\left(\begin{array}{cccc} I_{\text{in}} \rightarrow I_{\text{meas}} & Q_{\text{in}} \rightarrow I_{\text{meas}} & U_{\text{in}} \rightarrow I_{\text{meas}} & V_{\text{in}} \rightarrow I_{\text{meas}} \\ I_{\text{in}} \rightarrow Q_{\text{meas}} & Q_{\text{in}} \rightarrow Q_{\text{meas}} & U_{\text{in}} \rightarrow Q_{\text{meas}} & V_{\text{in}} \rightarrow Q_{\text{meas}} \\ I_{\text{in}} \rightarrow U_{\text{meas}} & Q_{\text{in}} \rightarrow U_{\text{meas}} & U_{\text{in}} \rightarrow U_{\text{meas}} & V_{\text{in}} \rightarrow U_{\text{meas}} \\ I_{\text{in}} \rightarrow V_{\text{meas}} & Q_{\text{in}} \rightarrow V_{\text{meas}} & U_{\text{in}} \rightarrow V_{\text{meas}} & V_{\text{in}} \rightarrow V_{\text{meas}} \end{array} \right)$$

CoMP-S pol. calibration results

- What is good and what bad? The measure is:
 - normalized $(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$ intensity differences
 - with a help of the obtained values of the physical parameters: linear polarizer transmission, circular retarder transmission & retardation Stokes_input vector, efficiencies (and other additional parameters)
 - Not the O matrix components...
- Results could be dependent on:
 - Position within the 2D field of view
 - Wavelength
 - other effects (e.g., mechanical structure bending, optical parts clearness)
- Results for 1 wavelength & 1 position in the FoV in this presentation

CoMP-S pol. calibration results

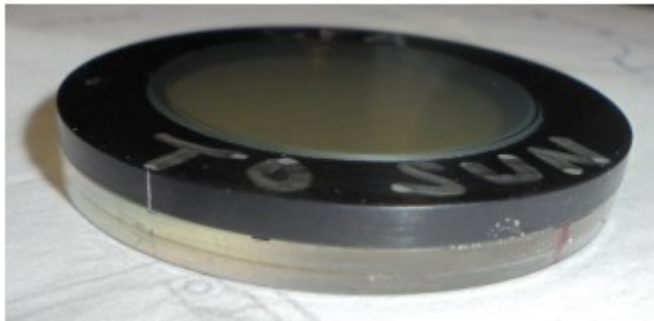
- Original CoMP-S setup & 656 nm: $(I_{\text{meas}} - I_{\text{model}})/I_{\text{mea}}$

0.00451119	0.000101250	5.81984e-06	-0.00473855
0.0213082	0.0573907	-0.0331494	-0.0306067
-0.0416938	-0.00697888	0.00598805	0.0341834
0.00717691	0.000137868	-0.00244441	-0.00689037
0.00280571	0.000276429	-0.00302491	-0.00267990
0.0914081	0.0443865	-0.0284551	-0.125710
0.141429	0.0337479	-0.0249009	-0.205270

- Something is wrong...
- Possible reason(s):
 - Reality: “wrong” optical parts ?
 - Model : insufficient description of the optical system ?
- Step by step checks/tests/analysis/re-considerations...

CoMP-S pol. calibration results

- Checks: calibration polarimetric optics: type, properties, orientation
→ lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder @ $+45^\circ$; lin. polarizer 0° + $\frac{1}{4}$ wave retarder @ -45° : orientation changes – unclear situation (really $\pm 45^\circ$?)

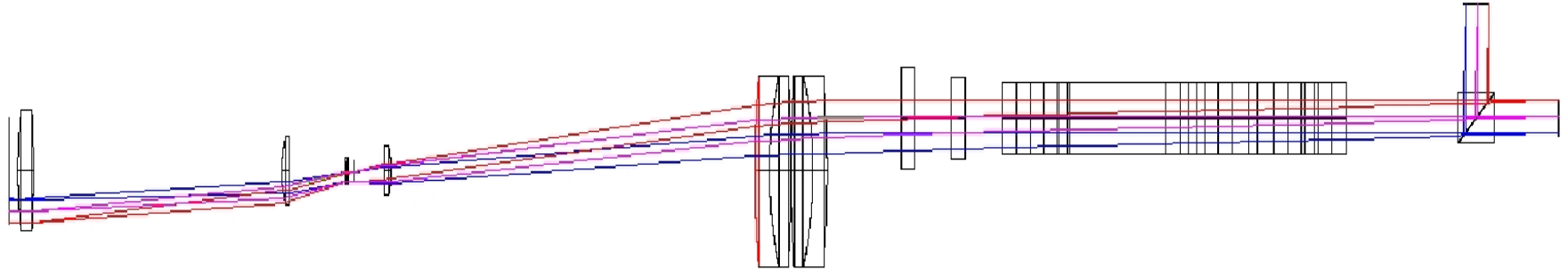


CoMP-S pol. calibration results

- Reconsiderations: CoMP-S “tertiary” optics - dichroich mirror @ 45° + polarizing beam splitting cube
- Tests: model apatation for these 2 optical elements:
 - The dichroic mirror MM analytical form (the free value of the refractive idex): *Collett, E., 1971, Am. J. Phys. 39, 517*
 - The polarizing beam splitter MM analytical form (birefringence and retardation – both linear and circular, depolarization, with few simplifications): *Song Zhang et al., 2018, J. Opt. 20, 125606*
- No significal inprovement of results $(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$

CoMP-S pol. calibration results

- Reconsiderations: the ZEISS coronagraph “secondary” optics (SO)

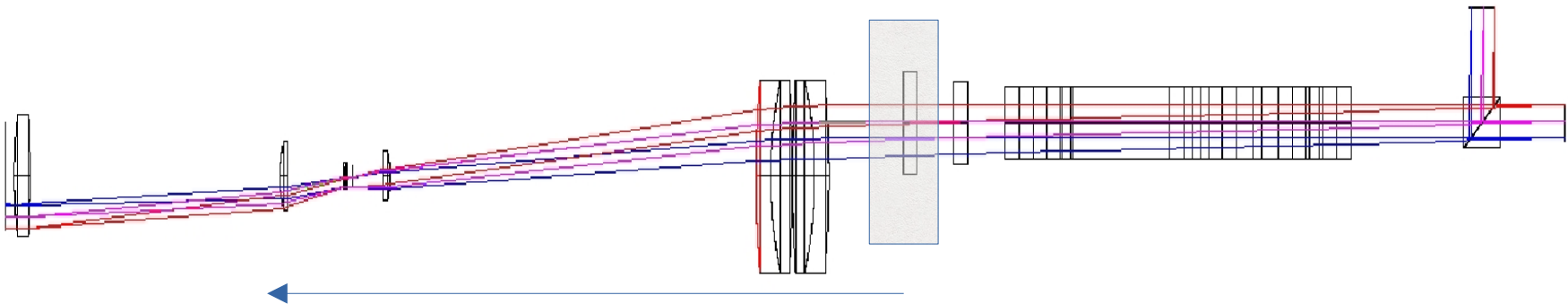


coronagraph secondary optics * CoMP-S instrument
field lens 3 lenses 4-lens objective cal.+ filt. wheels Lyot filter ter. optics

- Polarimetric effects of the single optical surface (without a symmetry of illumination): the Fresnel equations
- the quiet complex ZEISS coronagraph secondary optics changes the polarimetric status of the passing light

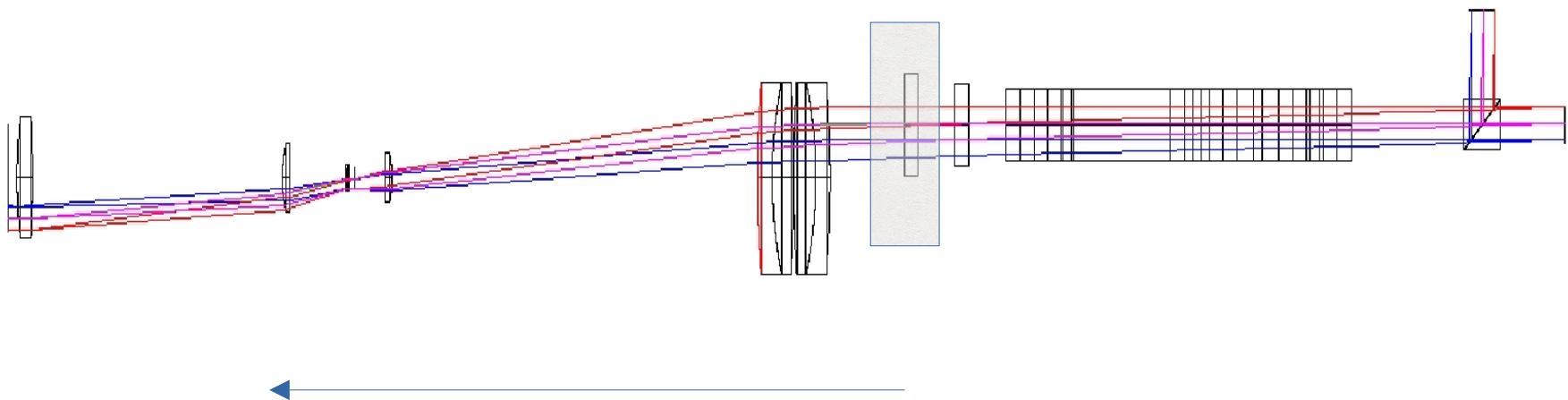
CoMP-S pol. calibration results

- **A conceptual problem of the instrument:** the complex ZEISS coronagraph secondary optics (SO) changes the polarimetric status of the passing light
- **So far:** an assumption of the completely unpolarized light $[I,Q,U,V]=[1,0,0,0]$ entering the polarimetric calibration optics...
- **A realistic solution:** placing the polarimetric calibration optics in front of the SO, i. e., where the artificial moon is located !



CoMP-S pol. calibration results

- **The realistic solution:** placing the polarimetric calibration optics in front of the SO, i. e., where the artificial moon is located
- Assumption: the completely unpolarized light $[I,Q,U,V]=[1,0,0,0]$ entering the polarimetric calibration optics is fulfilled
- Model has to be extended for the SO part – O_{SO} matrix (4x4):
 - observations: $O_{\text{common}} = O_{\text{CoMP-S}} \# O_{SO}$
 - pol. calibration measurements: $O_{\text{common}} = O_{\text{CoMP-S}} \# O_{\text{pol_cal}} \# O_{SO}$



CoMP-S pol. calibration results

- Analytical problem: 28 measurements but 31 unknown variables to be derived (O_{SO} 4x3 + pol. optics 3 + Input 4 + O_{CoMP-S} matrix 4x3)
- Numerical solutions:
 - a/ simplifications
28 measurements but 31 unknown variables to be derived (O_{SO} 4x3 + pol. optics 3 + Input 4 + O_{CoMP-S} matrix 4x3)
→
28 measurements and at maximum 28 unknown variables to be derived (O_{SO} 4x3 + pol. optics 3 + Input 4 + O_{CoMP-S} matrix at maximum 9 only)
 - b/ an iterative approach

CoMP-S pol. calibration results

- Preparation of a testing pol. calibration package #1:
 - Thorlabs lin. polarizer with variable orientation
 - lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder @ $+45^\circ$; lin. polarizer 0° + $\frac{1}{4}$ wave retarder @ -45° (HAO CPA/B parts)
 - in front of the SO – simplified approach - test data 2023/09/15
 - Results: $(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$ (optics: 0.67 & 0.84, 65.95)

-0.001	-0.002	0.002	0.001
-0.099	-0.008	-0.001	0.055
0.025	0.049	-0.035	-0.047
-0.006	0.008	0.019	-0.007
-0.004	0.011	0.014	-0.004
0.118	0.042	-0.012	-0.193
0.212	0.027	-0.009	-0.324

CoMP-S pol. calibration results

- Preparation of a testing pol. calibration package #2:
 - Thorlabs lin. polarizer with variable orientation
 - Thorlabs lin. polarizer @ 0° + ¼ wave retarder for 670 nm @ +/- 45°
 - in front of SO – simplified approach - test data 2023/10/14
 - Results: $(I_{\text{meas}} - I_{\text{model}})/I_{\text{meas}}$

-0.017	0.007	-0.005	0.016
0.025	-0.012	-0.017	-0.018
0.003	-0.072	-0.142	-0.006
0.165	0.039	-0.156	0.065
0.071	0.006	-0.077	-0.018
-0.056	0.016	-0.010	0.046
0.084	-0.041	0.035	-0.103



CoMP-S pol. calibration results

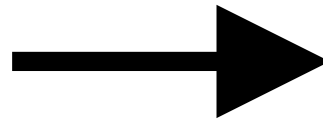
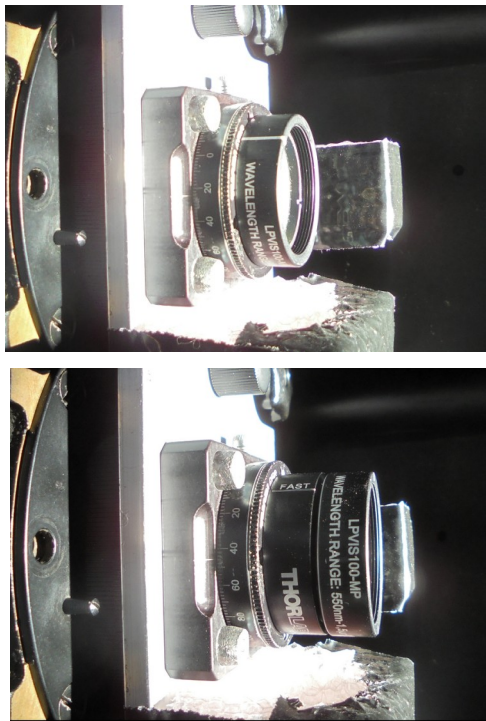
- Preparation of a testing pol. calibration package #2:
 - Thorlabs lin. polarizer with variable orientation
 - Thorlabs lin. polarizer @ 0° + $\frac{1}{4}$ wave retarder for 670 nm @ +/- 45°
 - in front of SO – simplified approach - test data 2023/10/14
 - Results:
 - linear polarizes trans = 0.26
 - $\frac{1}{4}$ wave retarder trans/ret = 0.97/90.6
 - O matrices: $O_{\text{CoMP-S}}$ & O_{SO}

1.00	-0.58	-0.06	0.29	1.00	0.53	0.10	0.10
1.00	0.71	0.73	-0.02	1.00	-1.03	0.05	0.04
1.00	0.72	0.49	0.08	1.00	-2.69	1.00	0.10
1.00	-0.28	-0.06	0.34	1.00	-3.55	0.65	0.68

CoMP-S pol. calibration results

- A (preliminary) summary:

It is needed to develop and fabricate an optimum achromatic pol. calibration package (500-1100 nm) which can be placed in front of the SO

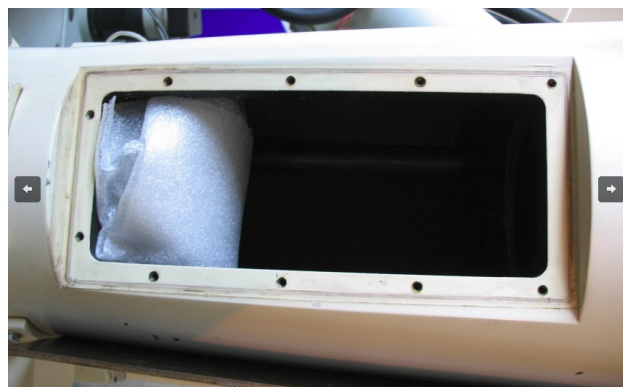


A new CoMP-S pol. package

- Requirements:
 - Placement in front the SO
 - Achromatic properties (500-1100 nm)
 - Versatile: in/out of the optical system allowing to exchange the artificial moon and to be placed to any location (position angle) around the solar limb
 - Computer controlled motorized operation
- Limitations:
 - Space & money
- Minimum content:
 - Achromatic linear polarizer - 4 orientations (0° , 90° , $+45^\circ$, -45°)
 - Achromatic $\frac{1}{4}$ wave retarder - 2 orientations ($+45^\circ$, -45°)

A new CoMP-S pol. package

- A preliminary concept:
 - Single linear polarizer rotatable to 4 orientations
 - Single achromatic $\frac{1}{4}$ wave retarder rotatable to 2 orientations
 - 2 rotatable platforms to place these pol. calibration optical parts to the required PA
 - Platform #1: 1 linear polarizer, #2: $\frac{1}{4}$ wave retarder + 1 hole
 - The whole package has to be removable from the coronagraph
 - Computer controlled motorized operation



CoMP-S polarization plan

- The iterative approach to derive the $O_{\text{CoMP-S}} + O_{\text{SO}}$ matrices – JR (now in progress)
- The preliminary summary → the final decision – JR + the LSO group
- Polarimetric calibration and demodulation to the CoMP-S data pipeline - JR
- the new polarization package: project, realization, tests → regular usage – the LSO group

Who what?

- S. Tomczyk:
 - CoMP-S polarimeter design
 - model approach software: basics
 - some advice
- The LSO group:
 - discussions and suggestions: P. Schwartz, P. Gomory, ...
 - mechanical parts, help with handling optics: M. Trembac
 - operation of the LSO and its instruments CoMP-S + UJ2P + ...
- JR:
 - polarimetric test measurements
 - model approach software: extensions
 - data analysis → results
 - new pol. calibration package concept and the polarimetry plan

Thank you for your attention

CoMP-S pol. demodulation

- The solar spectroscopy gold standard since the year 2000: del Toro Iniesta and Collados, "Optimum modulation and demodulation matrices for solar polarimetry", 2000, *Applied Optics* **39**, 1637

$$\mathbf{I}_{\text{meas}} = \mathbf{O}\mathbf{I}_{\text{in}} \quad \mathbf{I} \equiv (I, Q, U, V)^T$$

$$\mathbf{I}_{\text{in}} = \mathbf{D}\mathbf{I}_{\text{meas}}$$

$$\mathbf{D} = (\mathbf{O}^T\mathbf{O})^{-1}\mathbf{O}^T = \mathbf{A}^{-1}\mathbf{O}^T$$

CoMP-S polarization tests

- **List of the pol_cal (test) measurements:** the data analysis performed

Calibration optics type	Calibration optics location	Date	Position angle [°]
HAO CPA+CPB (CPA/B lin.pol. radially)	between SO and LF (calibration wheel)	(>27/04/2023) 2023/05/09 2023/05/10 2023/05/27	(~90) 105 105 105
HAO CPA+CPB (CPA/B lin.pol. radially)	in front of the SO (special holder)	(>19/07/2023) 2023/08/11 2023/09/06 2023/09/15	(90) 90 90 90
THORLABS lin_pol + wave/4	between SO and LF (calibration wheel)	-	-
THORLABS lin_pol + wave/4	In front of the SO (special holder)	2023/10/14 1w 2023/11/22 2w	90 90

LSO pipeline: done

- HAO (ST) soft + LSO (JR) fitting to derive the pol_cal modulation:

- pol_cal calibration optics definition:

```
;pol= [0, 1, 1, 1, 1, 1, 1] ; pol determines whether polarizer is present
;ret= [0, 0, 0, 0, 0, 1, 1] ; ret determines whether retarder is present
p_angle=[0., 0., 90., 45., 135., 0., 0.] ; pol angles
r_angle=[0., 0., 0., 0., 0., 45., -45.] ; ret angles
```

- Calculation of the calibration optics impact on the passing light:

```
if pol[i] eq 0 and ret[i] eq 0 then begin ; clear
  obs[* ,i] = omx ## input
endif
if pol[i] eq 1 and ret[i] eq 0 then begin ; polarizer only
  obs[* ,i] = omx ## mueller_partial_polarizer(ptrans,pp,p_angle[i]) ## input
endif
if pol(i) eq 1 and ret(i) eq 1 then begin ; retarder and polarizer
  obs[* ,i] = omx ## mueller_retarder(rtrans,r_angle[i],delta) ## $
  mueller_partial_polarizer(ptrans,pp,p_angle[i]) ## input
endif
```

LSO pipeline: done

- **Test data:** THORLABS lin.pol. + wave/4 @ in front of SO: 2023/10/14 & **model variants:** no adds, SO simplified, TO: PBS, TO: DM+PBS

no adds	SO simplified				TO: PBS				TO:DM+PBS						
$(i_obs-model)/(i_obs)$															
-0.045	0.023	-0.010	0.036	-0.034	0.010	0.001	0.022	-0.039	0.014	0.000	0.023	-0.036	0.014	0.001	0.022
0.027	-0.010	-0.017	-0.016	0.082	-0.004	0.005	-0.003	0.085	-0.000	0.006	0.007	0.079	-0.003	0.004	0.006
0.005	-0.061	-0.148	-0.007	0.018	-0.043	0.095	0.012	0.022	-0.019	0.113	0.021	0.019	-0.039	0.089	0.017
0.174	0.037	-0.161	0.052	0.013	0.030	-0.068	-0.075	0.009	0.015	-0.076	-0.075	0.005	0.028	-0.071	-0.073
0.061	0.011	-0.093	-0.007	0.017	0.034	-0.051	-0.031	0.009	0.039	-0.060	-0.029	0.014	0.030	-0.057	-0.029
-0.035	0.010	0.002	0.025	-0.015	-0.026	0.030	0.009	-0.008	-0.032	0.028	0.008	-0.015	-0.024	0.029	0.010
0.052	-0.034	0.021	-0.052	0.029	-0.040	0.034	-0.026	0.010	-0.030	0.032	-0.012	0.022	-0.039	0.031	-0.014
Pol.trans, Ret.trans Ret:															
0.53	0.97	90.62		0.57	0.86	81.94		0.57	0.86	81.56		0.57	0.86	81.78	
Input Stokes Vector:															
1.26	0.04	-0.44	-0.82	1.23	0.22	-0.33	-0.52	1.25	0.23	-0.31	-0.48	1.36	0.25	-0.35	-0.53
O Matrix:															
1.00	-0.58	-0.07	0.28	1.04	-0.71	-0.10	0.25	1.01	-0.69	-0.12	0.23	0.93	-0.64	-0.09	0.22
1.00	0.72	0.73	-0.01	0.87	0.56	0.60	0.00	0.84	0.54	0.57	0.01	0.78	0.50	0.54	0.00
1.00	0.73	0.50	0.07	0.83	0.59	0.34	0.06	0.80	0.57	0.31	0.06	0.74	0.53	0.30	0.05
1.00	-0.29	-0.05	0.38	1.00	-0.41	-0.09	0.38	0.97	-0.40	-0.11	0.37	0.89	-0.37	-0.09	0.34
Efficiencies:															
0.108	0.157	0.053	0.037	0.173	0.195	0.076	0.053	0.198	0.192	0.081	0.058	0.162	0.176	0.069	0.049
Efficiencies MAX:															
1.000	0.606	0.445	0.240	0.938	0.577	0.352	0.228	0.907	0.561	0.336	0.220	0.841	0.518	0.313	0.205
Chisq: 0.00108556															
				0.000362365				0.000368211				0.000357809			
d_mx ## [1.,1.,1.,1.]															
1.00	0.00	-0.00	-0.00	1.14	0.23	-0.19	-0.17	1.16	0.24	-0.16	-0.11	1.25	0.25	-0.18	-0.13
I				I				I				I			
1.01	0.01	-0.03	-0.03	1.15	0.24	-0.21	-0.19	1.16	0.25	-0.18	-0.13	1.26	0.27	-0.20	-0.15
Q				Q				Q				Q			
0.06	1.33	-0.03	-0.05	0.25	1.37	0.02	-0.07	0.26	1.40	0.04	-0.05	0.28	1.52	0.04	-0.05
U				U				U				U			
-0.67	-0.19	1.84	0.53	-0.43	-0.04	1.54	0.14	-0.38	-0.04	1.52	0.06	-0.47	-0.05	1.71	0.13
V				V				V				V			
-0.31	-0.03	0.51	2.30	-0.07	0.01	0.11	1.69	-0.03	0.01	0.02	1.58	-0.07	0.01	0.10	1.82
o_mx ## input_stokes_vector															
1.040	0.979	1.016	0.961	1.029	0.993	1.005	0.974	1.034	0.988	1.006	0.973	1.031	0.988	1.005	0.974